

Semi-Annual Status Report

DEVELOPMENT OF AN ENGINEERING
MODEL ATMOSPHERE FOR MARS

(SPECIAL TASK UNDER PROJECT ENTITLED "IMPROVEMENTS IN THE
PERTURBATION SIMULATIONS OF THE GLOBAL REFERENCE ATMOSPHERIC MODEL")

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Abstract

An engineering model atmosphere for Mars is being developed with many of the same features and capabilities of the highly successful Global Reference Atmospheric Model (GRAM) program for Earth's atmosphere (including mean values for density, temperature, pressure, and wind components, and density perturbation magnitudes and random perturbation profiles for density variations along specified trajectories). As an initial approach, the model is being built around the Martian atmosphere model computer subroutine (ATMOS) of Culp and Stewart (1984). In a longer-term program of research, additional refinements and modifications will be included. ATMOS includes parameterizations to simulate the effects of solar activity, seasonal variation, diurnal variation magnitude, dust storm effects, and effects due to the orbital position of Mars. One of the current shortcomings of ATMOS is the neglect of surface variation effects (with the exception of dust storm effects on the surface layer which are currently assumed to occur always with the same magnitude and at the same time every Martian "year"). The longer-term period of research and model building is to address some of these problem areas and provide further improvements in the model (including improved representation of near-surface variations, improved latitude-longitude gradient representation, effects of the large "annual" variation in surface pressure because of differential condensation/sublimation of the CO₂ atmosphere in the polar caps, and effects of Martian atmospheric wave perturbations on the magnitude of the expected density perturbations).

INTRODUCTION AND BACKGROUND

A highly successful and well-utilized engineering model for the Earth's atmosphere, the Global Reference Atmospheric Model (GRAM), has been developed at Georgia Tech (Justus, et al., 1980, 1986), and has undergone several improvement cycles. The GRAM program is used by several NASA Centers (and numerous other government agencies, industries and universities) for such projects as the Space Shuttle, the Space Station, Space Telescope, Tethered Satellite and AeroassistedOrbital Transfer Vehicle (AOTV). GRAM applications include orbital mechanics and lifetime studies, vehicle design and performance criteria, attitude control analysis problems, analysis of effects of short-term density variation from geomagnetic storms, and aerobraking analyses (for AOTV return from geosynchronous orbit to space-station rendezvous).

In addition to evaluating the mean density, temperature, pressure, and wind components at any height, latitude, longitude and monthly period, GRAM also allows for the simulation of "random perturbation" profiles about the mean conditions. This feature permits the simulation of a large number of realistic density profile realizations along the same trajectory through the atmosphere, with realistic values of scales of variation and peak perturbation values (e.g. the random perturbation profiles produce values which exceed the +3 standard deviation value approximately 1% of the time).

An engineering model atmosphere for Mars is being developed with many of the same features and capabilities of the GRAM program for Earth's atmosphere (including mean values for density, temperature, pressure, and wind components, and density perturbation magnitudes and random perturbation profiles for density variations along specified trajectories). As an initial approach, the model is being built around the Martian atmosphere model computer subroutine (ATMOS) of Culp and Stewart (1984). In a longer-term program of research and model-building, additional refinements and modifications will be included.

The ATMOS subroutine of Culp and Stewart incorporates results from a number of data and model sources, e.g. the Mars Reference Atmosphere (Kliore, 1982), occultation data and mass spectrometer data from Mariner and from Viking orbiters (Fjeldbo et al., 1966, 1970, 1977; Kliore et al., 1972; Stewart et al., 1972; Nier and McElroy, 1977), and data from the Viking lander atmospheric entry trajectories (Seiff and Kirk, 1977). ATMOS includes parameterizations to simulate the effects of solar activity, seasonal variation, diurnal variation magnitude, dust storm effects, and effects due to the orbital position of Mars.

One of the current shortcomings of ATMOS is the neglect of surface variation effects (with the exception of dust storm effects on the surface layer which are currently assumed to occur always with the same magnitude and at the same time every Martian "year").

PROGRAM OF RESEARCH

An engineering model atmosphere, similar to GRAM for the Earth's atmosphere, is being developed for Mars. Initially the model will be built around the ATMOS subroutine of Culp and Stewart (1984), which allows simulation of mean density, high and low density perturbation magnitudes, temperature and pressure at any altitude, areographic position and Martian season. Some features which have been added are methods to simulate mean wind components and random perturbation density profiles along specified trajectories.

Specific modifications and additions to the ATMOS subroutine and/or features of the new main program also include:

- (1) Modification to latitude, longitude, and height input, and solar latitude, longitude, and Mars orbital radius input to the ATMOS subroutine. The original ATMOS routine required areocentric Cartesian coordinate (x-y-z) input values of these parameters. This change will make input to the program and operation of the program more similar to that for GRAM.
- (2) A parameterization of the orbital parameters of Mars (from ephemeris data), so that these can be evaluated by the program, instead of input from separate ephemeris look-up results for each simulation case. The original ATMOS required the areocentric coordinates of the sun and the Julian date to be input. All of these are now evaluated from input of the calendar date (Earth-based Universal Time) and Greenwich time for which simulations are to be made. No solar or Martian orbital parameters are required among the input supplied by the user. The parameterization of the necessary orbital parameters was based on ephemeris data from 1976 through 1988, to provide appropriate accuracy during at least this period.
- (3) Parameterizations for horizontal and vertical scales of density perturbations as a function of height have been developed, for use in the

random perturbation model for density.

- (4) Trajectory options (similar to GRAM) have been implemented whereby atmospheric parameters along linear steps in height, latitude and/or longitude can be simulated, or simulations can be made along any desired trajectory for which height-latitude-longitude positions are provided in an input data file.
- (5) Simulation of mean wind components from mean pressure gradient and other factors has been added. Preliminary results from ATMOS indicate that above 100 km or so, the areostrophic winds (analogous to geostrophic winds, computed by a balance of pressure gradient and coriolis forces) become much too large. An areostrophic wind simulation technique including the damping effects of molecular viscosity (which becomes large at low density and high temperature) has therefore been included (similar to the viscous model at high altitudes recently added to the GRAM program).

All of these modifications and additions have been incorporated into an IBM-PC-DOS-compatible computer program (written in FORTRAN), the listing for which is given in the Appendix.

Figures 1 and 2 show sample output from the current MARS/ATMOS program. These are vertical profiles of density and temperature at the latitude-longitude position of the Viking 1 lander for the day of its landing. These may be compared with similar figures given by Culp and Stewart (1984).

PLANS FOR THE LONGER-TERM PROGRAM OF RESEARCH

One of the current shortcomings of ATMOS is the neglect of surface variation effects (with the exception of dust storm effects on the surface layer which are currently assumed to occur always with the same magnitude and at the same time every Martian "year"). The longer-term research and model development period will address some of these problem areas and provide further improvements in the model, including improved representation of near-surface variations, improved latitude-longitude gradient representation, and effects of Martian atmospheric wave perturbations. Specific areas of study and program improvements expected during this research and model-building period will include:

- (1) Improvement in the treatment of surface and near-surface effects of seasonal and diurnal variations. Data from the Viking landers (Hess et al., 1977, 1980) will be analyzed and used, as well as results from theoretical studies of surface solar heating and expected resultant near-surface temperature variations and thermal wind patterns (e.g. Leovy and Mintz, 1969).
- (2) Improvement in the latitude-longitude gradients of temperature, pressure, and density in the Martian troposphere (surface to about 40 km). Preliminary studies with ATMOS indicate that this routine significantly underestimates the latitude gradient of temperature and pressure (and hence the build up of tropospheric winds by the thermal wind gradient (vertical variation of the areostrophic wind)).
- (3) Inclusion of the effects of seasonal variations in the total mass of the Martian atmosphere, as different amounts of CO₂ are condensed at one pole and sublimed at the other, during the different Martian seasons. This effect is evident in the large ($\approx 30\%$) annual variations of surface pressure measured at the Viking Lander sites (Hess, et al., 1980). The present ATMOS routine uses a fixed value of surface pressure (6.1 mb), independent of season.
- (4) Addition of time of year and magnitude selection for dust-storm perturbations. Presently ATMOS assumes a fixed magnitude dust storm which re-occurs during the same period of every Martian "year". The dust storm effects are currently treated by producing an isothermal layer at the Martian surface, with the higher thermal layers pushed upward by the same amount. The program will be modified so that the intensity of the dust-storm effect and the period of its occurrence can be selected by program input parameters.

A major activity of the extended period of research (to be conducted by co-investigator, Dr. George Chimonas) will be an analysis of the expected effects on density perturbation magnitudes due to wave phenomena in the Martian atmosphere. In the Earth's atmosphere, various wave phenomena (including planetary waves, tides, gravity waves, lee waves, etc.) are responsible for a substantial part of the atmospheric variability above the boundary layer. These

perturbation magnitudes which can be added in with those already treated in the ATMOS routine. These magnitudes will have a direct effect on the random perturbation model for profiles of density perturbation values along the selected trajectories.

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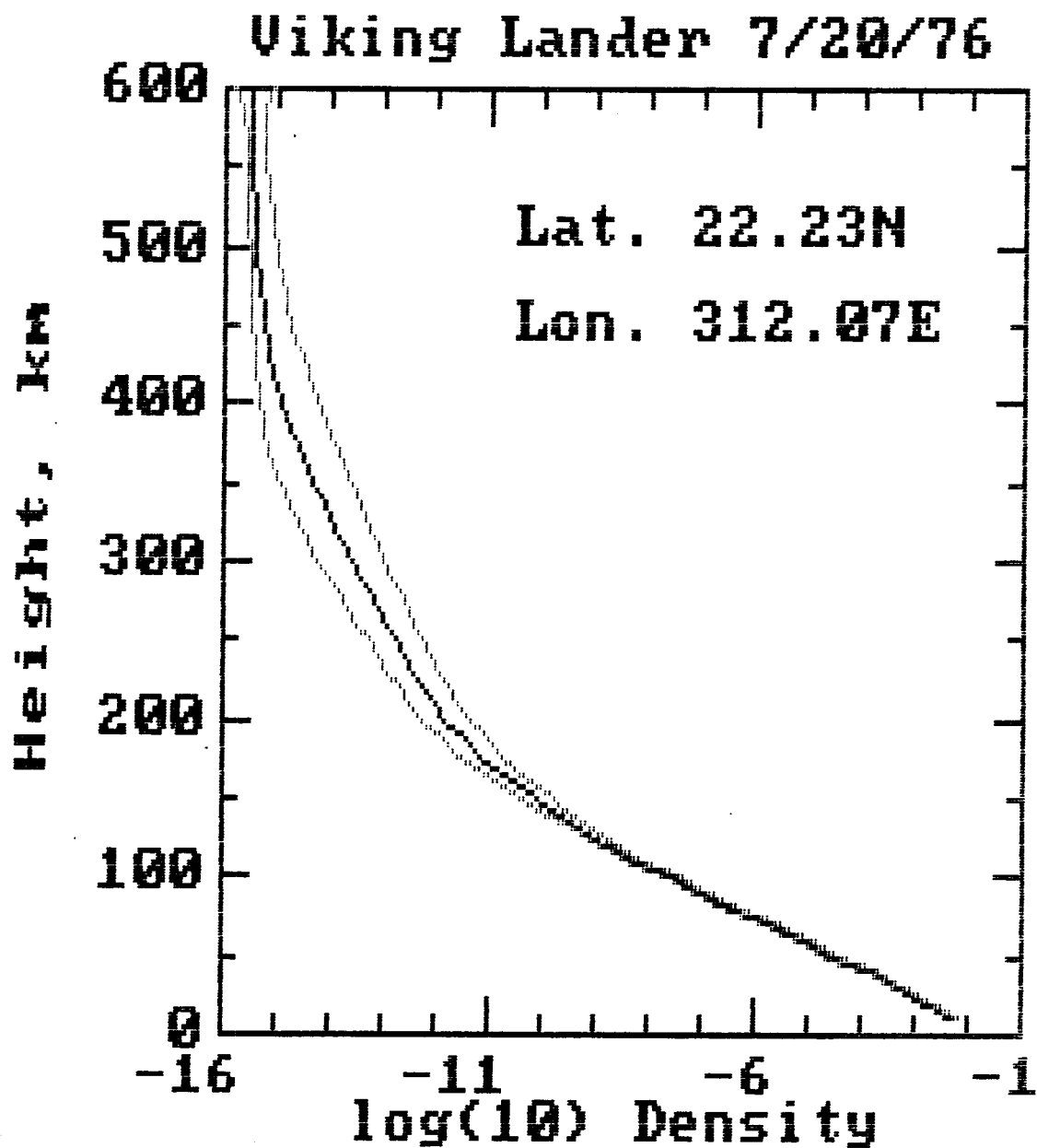


Figure 1 - Simulated density profile (log-base-10 scale, units kg/m^3) from the MARS/ATMOS program, for a vertical path at the position of the Viking 1 Lander.

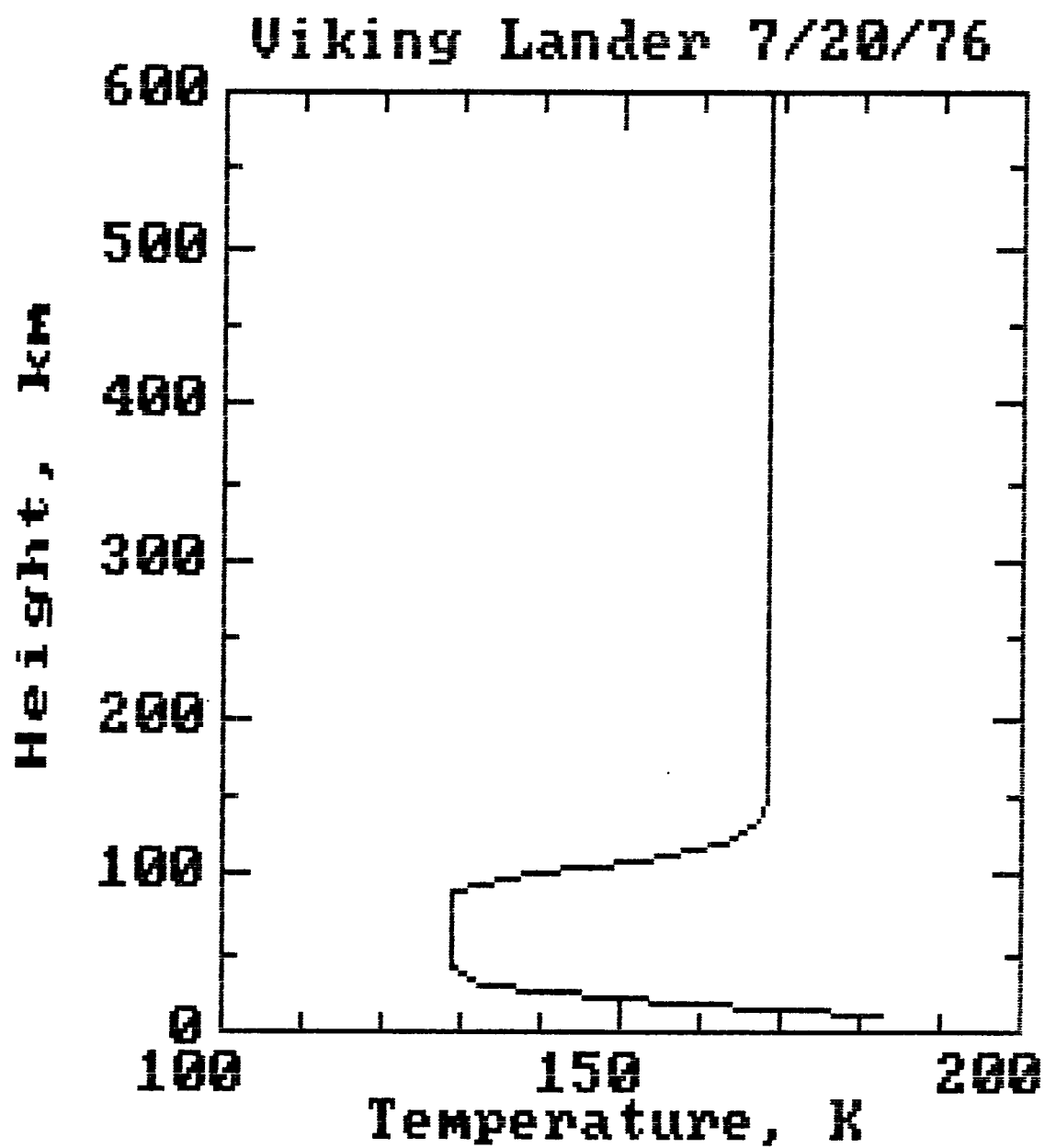


Figure 2 - As in Figure 1 for temperature.

APPENDIX A - MARS PROGRAM AND SUBROUTINE LISTINGS

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C....  PROGRAM MARS - program to evaluate density, temperature,
C      pressure and wind components at a given time and position in
C      the Martian atmosphere
C.....
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)
      DOUBLE PRECISION MARSAU,MARSRAD,NSWIND
      DIMENSION IDAY(12),IERR(10)
      character*8 lstfl,FILES(10),outfl
      EQUIVALENCE (IERR1,IERR(1)),(IERR2,IERR(2)),(IERR3,IERR(3)),
& (IERR4,IERR(4)),(IERR5,IERR(5)),(IERR6,IERR(6)),(IERR7,IERR(7))
& ,(IERR8,IERR(8)),(IERR9,IERR(9)),(IERR10,IERR(10))
      DATA files/'LIST','DENSLO','DENSAV','DENSHI','DENSRP','TEMP',
& 'PRES','EWWIND','NSWIND','OUTPUT'/
      DATA IDAY/0,31,59,90,120,151,181,212,243,273,304,334/
      write(*,120)
120    format(' Enter name for LIST file (CON for console listing): ')
      read(*,71)lstfl
71    format(A)
      files(1)=lstfl
      WRITE(*,124)
124    FORMAT(' Enter name for OUTPUT file:')
      read(*,71)outfl
      files(10)=outfl
      OPEN(8,file=lstfl,status='new',iostat=ierr1)
      OPEN(21,file='DENSLO',status='new',iostat=ierr2)
      OPEN(22,file='DENSAV',status='new',iostat=ierr3)
      OPEN(23,file='DENSHI',status='new',iostat=ierr4)
      OPEN(24,file='DENSRP',status='new',iostat=ierr5)
      OPEN(25,file='TEMP',status='new',iostat=ierr6)
      OPEN(26,file='PRES',status='new',iostat=ierr7)
      OPEN(27,file='EWWIND',status='new',iostat=ierr8)
      OPEN(28,file='NSWIND',status='new',iostat=ierr9)
      OPEN(29,file=outfl,status='new',iostat=ierr10)
      do 87 j=1,10
87    if(ierr(j).ne.0)goto 121
      goto 123
121    write(*,122)files(j)
122    format(a8,' Filename is old!')
      goto 9998
123    DTR = 1.74532925199d-2
C...  VISCOSITY OF CARBON DIOXIDE: COEFFICIENTS FROM DATA IN 'TABLES
C      OF PHYSICAL AND CHEMICAL CONSTANTS' BY G.W.C. KAYE & T.H. LABY,
C      1961, LONGMANS, GREEN & CO., LONDON
      BETA = 1.578d-6
      SVAL = 2.40D2
C...  DAY = SIDEREAL DAY; CORFAC = CORIOLIS FACTOR (EXCEPT FOR
C      LATITUDE EFFECT)
      DAY = 2.4622962D1
      CORFAC = DTR/(1.0d1*DAY)
C...  FACTORS FOR USE IN CORRELATION FUNCTION
      AFAC = 19.51615854016301d0
      BFAC = 1.00041693941245578d0

```

```

200  WRITE(*,500)
500  FORMAT(' Enter Month, Day of Month, 4-digit Year,',
&    ' and Max Number Positions ')
    READ(*,*)MONTH,MDAY,MYEAR,NPOS
    IF(MONTH.LE.0.OR.MONTH.GT.12)GOTO 9999
    WRITE(*,300)
300  FORMAT(' Enter initial GMT Time (Hours, Minutes, Seconds)')
    READ(*,*)IHR,IMIN,SEC
    IF(MYEAR.LT.1900)MYEAR = MYEAR + 1900
    IF(NPOS.GT.0) GOTO 330
    OPEN(7,file='TRAJDATA',iostat=ierr7)
    if(ierr7.ne.0) goto 310
    goto 330
310  write(*,320)
320  format(' Unable to open Trajectory Data file')
    goto 9998
330  MAXNUM = NPOS - 1
    IF(NPOS.LE.0)MAXNUM = 32000
    NDAY = IDAY(MONTH) + MDAY
    IF(MOD(MYEAR,4).EQ.0.AND.MONTH.GT.2)NDAY = NDAY + 1
    XYEAR = (MYEAR - 1.9665d3)/4.0d0
    DATE = 2.439856d6 + 3.65d2*(MYEAR - 1.968d3) + NDAY +
&    DINT(XYEAR + DSIGN(0.5d0,XYEAR))
    WRITE(8,550)MONTH,MDAY,MYEAR,DATE,IHR,IMIN,SEC
550  FORMAT(' Date = ',I2,'/',I2,'/',I4,' Julian Date = ',F9.0,
&    ' GMT Time = ',I2,':',I2,':',F4.1)
    DATE = DATE + IHR/2.4d1 + IMIN/1.440d3 + SEC/8.6400d4
    DATE0 = DATE
    WRITE(*,710)
710  FORMAT('/' Enter Starting Random Number (Any odd positive',
&    ' integer)')
    READ(*,*)NR1
    RHO = RAND(NR1)
    WRITE(8,720)NR1
720  FORMAT(' Starting random number = ',I6)
    WRITE(*,730)
730  FORMAT('/' Enter 1, 2 or 3 for output versus Height, Latitude',
&    ' , or Longitude, respectively')
    READ(*,*)NVAR
    IF(NVAR.LT.1.OR.NVAR.GT.3)NVAR = 1
    IF(NPOS.LE.0)GO TO 750
10  WRITE(*,100)
100  FORMAT(' Enter Initial Height (km), Latitude (deg.),',
&    ' Longitude (deg.)')
    READ(*,*)FHGT,FLAT,FLON
    IF(FHGT.LT.0.)GOTO 200
20  WRITE(*,700)
700  FORMAT(' Enter Increments in Height (km), Latitude (deg.),',
&    ' Longitude (deg.),'/' and Time (sec.)')
    READ(*,*)DELHGT,DELLAT,DELLON,DELTIME
750  WRITE(*,755)
755  FORMAT(' Computing data.')
    DO 900 I = 0,MAXNUM
    IF(NPOS.GT.0)GO TO 150
    READ (7,*,ERR=9998,END=200)CSEC,CHGT,CLAT,CLON
    DATE = DATE0 + CSEC/8.6400d4

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GO TO 160
150  CHGT = FHGT + I*DELHGT
      CLAT = FLAT + I*DELLAT
      CLON = FLON + I*DELLON
      CSEC = I*DELTIME
      DATE = DATE0 + CSEC/8.6400d4
160  IF(CHGT.LT.0.0)GO TO 200
      IF(DABS(CLAT).LE.90.d0)GO TO 170
      CLAT = DSIGN(1.80d2,CLAT) - CLAT
      CLON = CLON + 1.80d2
170  IF(CLON.LT.0.0)CLON = CLON + 3.60d2
      IF(CLON.GT.360.0) CLON = CLON - 3.60d2
      CALL ORBIT(DATE,SUNLAT,SUNLON,ALS,MARSAU)
      MARSRAD = MARSAU*1.496d+8
      CALL ATMOS(CHGT,CLAT,CLON,MARSRAD,SUNLAT,SUNLON,ALS,DATE,
&  HSCALE,TEMP,DENS,FACTHI,FACTLO,PRES,RSC)
      DENSLO = DENS*FACTLO
      DENSHI = DENS*FACTHI
      DPLUS = DENSHI - DENS
      DMINUS = DENS - DENSLO
      CALL NORMAL(Z1,Z2)
      CORREL = 0.
      VLS = 5.9d0 + 0.7d-01*CHGT**1.5d0
      IF(VLS.GT.CHGT.AND.CHGT.GT.1.35d2)VLS = CHGT
      IF(I.EQ.0)GO TO 180
      HLS = 1.350d3 + 9.0d0*CHGT
      IF(HLS.GT.6.750d3)HLS = 6.750d3
      DELNS = DTR*RSC*(CLAT - PLAT)/HLS
      DLON = CLON - PLON
      IF(DABS(DLON).GT.2.70d2)DLON = DSIGN(3.60d2,DLON) - DLON
      IF(DABS(DLON).GT.9.0d1)DLON = DLON - DSIGN(1.80d2,DLON)
      DELEW = DTR*RSC*DCOS(DTR*CLAT)*DLON/HLS
      DELZ = (CHGT - PHGT)/VLS
      DELX = DSQRT(DELNS**2 + DELEW**2 + DELZ**2)
      IF(DELX.LT.0.05d0)CORREL = 1.0d0 - AFAC*DELX**2
      IF(DELX.GE.0.05d0)CORREL = DEXP(-BFAC*DELX)
180  PHGT = CHGT
      PLAT = CLAT
      PLON = CLON
      RHO = CORREL*RHO + DSQRT(1.0d0 - CORREL**2)*Z1
      IF(RHO.LT.0.0)DENSP = DENS + RHO*DMINUS
      IF(RHO.GE.0.0)DENSP = DENS + RHO*DPLUS
      CALL ATMOS(CHGT,CLAT,CLON+2.5d0,MARSRAD,SUNLAT,SUNLON,ALS,DATE,
&  HLONP,TLONP,DLONP,FACTHI,FACTLO,PLONP,RLONP)
      CALL ATMOS(CHGT,CLAT,CLON-2.5d0,MARSRAD,SUNLAT,SUNLON,ALS,DATE,
&  HLONM,TLONM,DLONM,FACTHI,FACTLO,PLONM,RLONM)
      CLATP = CLAT + 2.5d0
      CLONP = CLON
      IF(CLATP.LE.9.0d1)GO TO 570
      CLATP = 1.80d2 - CLATP
      CLONP = CLONP + 1.80d2
570  CALL ATMOS(CHGT,CLATP,CLONP,MARSRAD,SUNLAT,SUNLON,ALS,DATE,
&  HLATP,TLATP,DLATP,FACTHI,FACTLO,PLATP,RLATP)
      CLATM = CLAT - 2.5d0
      CLONM = CLON
      IF(CLONM.GE.-9.0d1)GO TO 580

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```

      CLATM = -1.80d2 - CLATM
      CLONM = CLONM + 1.80d2
580    CALL ATMOS(CHGT,CLATM,CLONM,MARSRAD,SUNLAT,SUNLON,ALS,DATE,
      & HLATM,TLATM,DLATM,FACTHI,FACTLO,PLATM,RLATM)
      DELNS = DTR*RSC*5.0d3
      WLAT = CLAT
      IF(DABS(WLAT).GT.8.75d1)WLAT = DSIGN(8.75d1,WLAT)
      IF(DABS(WLAT).LT.2.5d0)WLAT = DSIGN(2.5d0,WLAT)
      DELEW = DTR*RSC*DCOS(DTR*WLAT)*5.0d3
      CORIOL = CORFAC*DSIN(DTR*WLAT)
      VISC = BETA*TEMP**1.5d0/(TEMP + SVAL)
      VISCFAC = VISC/(1.0d6*DENS*VLS**2)
      DPDY = (PLATP-PLATM)/(DELNS*DENS)
      DPDX = (PLONP-PLONM)/(DELEW*DENS)
      DENOM = CORIOL**2 + VISCFAC**2
      EWWIND = (-CORIOL*DPDY - VISCFAC*DPDX)/DENOM
      NSWIND = (CORIOL*DPDX - VISCFAC*DPDY)/DENOM
      WRITE(8,590)CSEC,CHGT,HSCALE,CLAT,CLON
590    FORMAT(' TIME (relative to initial time) = ',F12.1,' seconds'/
      & ' HEIGHT = ',F7.1,' km',13X,' SCALE HEIGHT = ',
      & F6.2,' km'/' LATITUDE = ',F8.3,' degrees      EAST LONGITUDE = ',
      & F8.3,' degrees')
      WRITE(8,600)TEMP,DENSLO,DENS,DENSHI,DENSP,PRES,
      & EWWIND,NSWIND
600    FORMAT(' TEMPERATURE = ',F7.1,' K'/
      & ' DENSITY (Low, Avg., High) = ',3G12.4,' kg/m**3'/
      & ' DENSITY PLUS PERTURBATION = ',G12.4,' kg/m**3'/
      & ' PRESSURE = ',G12.4,' N/m**2'/' EASTWARD WIND = ',F7.1,
      & ' m/s      NORTHWARD WIND = ',F7.1,' m/s')
      WRITE(8,650)
650    FORMAT(' -----',
      & '-----')
      IF(NVAR.EQ.1)VAR = CHGT
      IF(NVAR.EQ.2)VAR = CLAT
      IF(NVAR.EQ.3)VAR = CLON
      WRITE(21,890)VAR,Dlog10(DENSLO)
      WRITE(22,890)VAR,Dlog10(DENS)
      WRITE(23,890)VAR,Dlog10(DENSHI)
      WRITE(24,890)VAR,Dlog10(DENSP)
      WRITE(25,890)VAR,TEMP
      WRITE(26,890)VAR,Dlog10(PRES)
      WRITE(27,890)VAR,EWWIND
      WRITE(28,890)VAR,NSWIND
890    FORMAT(F10.3,G12.4)
      SIGD = 5.0d1*(DENSHI-DENSLO)/DENS
      WRITE(29,895)CHGT,CLAT,CLON,Dlog10(DENS),TEMP,EWWIND,NSWIND,SIGD
895    FORMAT(F5.1,7F7.2)
900    CONTINUE
      GOTO 200
9998   STOP ' Error Termination Reading Data File'
9999   STOP ' Normal Termination'
      END

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```

      subroutine orbit(xdate,ds,lon,ls,rad)
C...   Subroutine to compute Mars orbital parameters from input
C       Greenwich time (xdate, day and fraction).  Output consists of:
C       ds and lon - the areographic latitude and longitude of the sun,
C       ls - the heliocentric longitude of Mars (longitudinal angular
C       position of Mars around its orbital path, 0-360 degrees = one
C       Martian year), and
C       rad - the heliocentric orbital radius of Mars
C.....
      implicit double precision (a-h,o-z)
      double precision ls0,lon0,ls,lon
      data ls0,perls,TWOPI/6.36d0,6.8697964d2,6.28318530718d0/
      data lon0,perlon,fact/3.5758d2,1.02749118d0,0.9896538d0/
      data a0,a1,a2,a3,a4,a5,a6/1.5303331d0,.13661274d0,.38073649d-1,
&      -.34125165d-2,.56508078d-2,-.31633117d-3,-.33458978d-3/
      data b0,b1,b2,b3,b4,b5,b6/2.2057565d0,2.4703515d1,-1.5459399d0,
&      -0.50388237d0,2.2083870d0,-0.39583136d0,-0.077578018d0/
      data c0,c1,c2,c3,c4,c5,c6/-9.9300079d0,-2.8679217d0,1.0298739d1,
&      -0.53266474d0,-0.32173731d0,0.36206144d-1,-0.034765340d0/
      data d0,d1,d2,d3,d4,d5,d6/-3.5158255d0,6.5240771d0,-9.3284323d0,
&      1.9052424d0,2.4887938d0,-0.49182825d0,0.10130513d-1/
      perl=6.87D2/TWOPI
      per2=6.96D2/TWOPI
      PI180 = TWOPI/3.60d2
      DATE = XDATE - 2.442779d6
      xls = ls0 + 3.60D2*date/perl
      xlon = lon0 + 3.60D2*(date - 2.922D3)/perlon
      TIME1=DATE/PER1
      TIME2=DATE/PER2
      LS=C0+C1*DSIN(TIME1)+C2*DCOS(TIME1)+C3*DSIN(2.*TIME1)
&      +C4*DCOS(2.*TIME1)+C5*DSIN(3.*TIME1)+C6*DCOS(3.*TIME1)+XLS
      DS=B0+B1*DSIN(TIME1)+B2*DCOS(TIME1)+B3*DSIN(2.*TIME1)
&      +B4*DCOS(2.*TIME1)+B5*DSIN(3.*TIME1)+B6*DCOS(3.*TIME1)
      LON=D0+D1*DSIN(TIME2)+D2*DCOS(TIME2)+D3*DSIN(2.*TIME2)
&      +d4*Dcos(2.*time2)+d5*Dsin(3.*time2)+d6*Dcos(3.*time2)
&      +xlon
      LS = DMOD(LS,3.6D2)
      LON = DMOD(LON,3.6D2)
      if(ls.lt.0.)ls = ls + 3.60D2
      if(lon.lt.0.)lon = lon + 3.60D2
      rad = a0 + a1*Dsin(timel) + a2*Dcos(timel) + a3*Dsin(2.*timel)
&      + a4*Dcos(2.*timel) + a5*DSin(3.*timel) + a6*Dcos(3.*timel)
      RETURN
      end

      SUBROUTINE ATMOS (CHGT,CLAT,CLON,MARSRAD,SUNLAT,SUNLON,ALS,
&      DATE,H,TEMP,DENST,UPFCTR,LWFCTR,PRES,RSC)
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)

C
C       CHGT      HEIGHT OF SPACECRAFT ABOVE REFERENCE SURFACE (KM)(INPUT)
C       CLAT      LATITUDE OF SPACECRAFT (DEGREES) (INPUT)
C       CLON      LONGITUDE OF SPACECRAFT (DEGREES) (INPUT)
C       MARSRAD   MARS ORBITAL RADIUS (KM) (INPUT)

```

C SUNLAT AEROCENTRIC LATITUDE OF SUN (DEGREES) (INPUT)
C SUNLON AEROCENTRIC LONGITUDE OF SUN (DEGREES) (INPUT)
C ALS MARS LONGITUDE IN ORBIT (INPUT)
C DATE JULIAN DATE (INPUT)
C H SCALE HEIGHT AT SPACECRAFT POSITION (KM) (OUTPUT)
C TEMP TEMPERATURE AT SPACECRAFT POSITION (K) (OUTPUT)
C DENST MASS DENSITY AT SPACECRAFT POSITION (KG/M**3) (OUTPUT)
C UPFCTR UPPER DEVIATION FACTOR ON MASS DENSITY (OUTPUT)
C LWFCTR LOWER DEVIATION FACTOR ON MASS DENSITY (OUTPUT)
C PRES PRESSURE AT SPACECRAFT POSITION (N/M**2) (OUTPUT)
C RSC AEROCENTRIC RADIUS TO SPACECRAFT (KM) (OUTPUT)
C*****
C A SEMIMAJOR AXIS OF MARS ORBIT (KM)
C AH AVERAGE SCALE HEIGHT WHICH IS FUNCTION OF TINF (KM)
C AF MAJOR AMPLITUDE OF SOLAR WAVE
C AVOGDR RECIPROCAL OF AVOGADROS NUMBER (KG-MOLE)
C B MINOR AMPLITUDE OF SOLAR WAVE
C DL LONGITUDE DIFFERENCE BETWEEN SPACECRAFT AND SUN
C DT DIFFERENCE OF DATE BETWEEN PRESENT AND REFERENCE
C DTR CONSTANT CONVERTED DEGREE TO RADIAN
C DZDS INCREMENT OF ALTITUDE DUE TO DUST STORM (KM)
C DZSN INCREMENT OF ALTITUDE DUE TO SUN (KM)
C EB EXPONENTIAL CONSTANT FOR $Z_B < Z < Z_F$
C EL EXPONENTIAL CONSTANT FOR $Z_L < Z < Z_A$
C ED AMPLITUDE OF DIURNAL EFFECT (KM)
C ES AMPLITUDE OF SEASONAL EFFECT (KM)
C F(I) VECTOR STORED FRACTION OF EACH GAS AT Z_F
C F107 SOLAR FLUX AT 10.7 CENTIMETER WAVELENGTH
C FP FRACTION OF HELIOCENTRIC PERIOD
C G6 GRAVITY AT ALTITUDE Z_6 (CM/SEC**2)
C GL GRAVITY AT ALTITUDE Z_L (CM/SEC**2)
C GA GRAVITY AT ALTITUDE Z_A (CM/SEC**2)
C GB GRAVITY AT ALTITUDE Z_B (CM/SEC**2)
C GF GRAVITY AT ALTITUDE Z_F (CM/SEC**2)
C GFOKT PARAMETER EQUALS $10.*GF/(K*TINF)$
C H6 RECIPROCAL OF SCALE HEIGHT FOR $Z_6 < Z < Z_L$ (1/KM)
C HA RECIPROCAL OF SCALE HEIGHT FOR $Z_A < Z < Z_B$ (1/KM)
C HINF RECIPROCAL OF SCALE HEIGHT FOR HIGH ALTITUDE (1/KM)
C IC PARAMETER USED FOR SWITCHING TINF
C K UNIVERSAL GAS CONSTANT (J/KG-MOLE * K)
C MBAR AVERAGE MOLECULAR WEIGHT OF GASES
C MBOK PARAMETER EQUALS $10.*(MBAR/K)$
C MW(I) VECTOR STORED MOLECULAR WEIGHT OF EACH GAS
C NC NUMBER OF CONSTITUENT GASES
C NBDNS(I) VECTOR STORED NUMBER DENSITY OF EACH GAS (1/CM**3)
C WHERE I - 1 REPRESENTS CO2
C 2 REPRESENTS O
C 3 REPRESENTS N2
C 4 REPRESENTS AR
C 5 REPRESENTS CO
C 6 REPRESENTS O2
C 7 REPRESENTS HE
C 8 REPRESENTS H
C 9 REPRESENTS H2
C P PRESSURE AT SPACECRAFT POSITION (N/M**2)
C P6 PRESSURE AT Z_6 EQUALS 6.1 MILLIBAR


```

C   PA      PRESSURE AT ZA (N/M**2)
C   PB      PRESSURE AT ZB (N/M**2)
C   PL      PRESSURE AT ZL (N/M**2)
C   PF      PRESSURE AT ZF (N/M**2)
C   PP(I)   VECTOR STORED PARTIAL PRESSURE OF EACH GAS
C   PERIOD  SIDEREAL PERIOD OF MARS (DAYS)
C   R61MB   AREOCENTRIC DISTANCE OF 6.1-MILLIBAR SPHEROID (KM)
C   RA      SEMIMAJOR AXIS OF ATMOSPHERIC ELLIPSOID (KM)
C   RB      SEMIMINOR AXIS OF ATMOSPHERIC ELLIPSOID (KM)
C   RC      POLAR AXIS OF ATMOSPHERIC ELLIPSOID (KM)
C   REFDAT  DATE OF MARS PERIHELION
C   RSC     AREOCENTRIC DISTANCE OF SPACECRAFT (KM)
C   RSN     HELIOCENTRIC DISTANCE OF MARS (KM)
C   RSQ     DUMMY VARIABLE FOR CALCULATING R61MB
C   SCLAT   LATITUDE OF SPACECRAFT (RAD.) (ROTATING COORDINATES)
C   SCLONG  LONGITUDE OF SPACECRAFT (RAD.)
C   SNLAT   LATITUDE OF SUN (RAD.) (ROTATING COORDINATES)
C   SNLONG  LONGITUDE OF SUN (RAD.)
C   SIGMA   ESTIMATED STANDARD DEVIATION PARAMETER
C   SOLDAY  DAYS IN EARTH YEAR
C   TF      TEMPERATURE AT THERMOSPHERIC SURFACE (K)
C   T       TEMPERATURE AT SPACECRAFT POSITION (K)
C   T6      TEMPERATURE AT ALTITUDE Z6
C   TA      TEMPERATURE AT ALTITUDE ZA      (K)
C   TB      TEMPERATURE AT ALTITUDE ZB
C   TIME    LOCAL TIME AT SPACECRAFT POSITION (RAD.)
C   TPL     RATE OF CHANGE OF TEMP. FOR ZL < Z < ZA (K/KM)
C   TPB     RATE OF CHANGE OF TEMP. FOR ZB < Z < ZF (K/KM)
C   TINF    EXOSPHERIC TEMPERATURE (K)
C   U       UNIVERSAL GRAVITATIONAL CONSTANT (CM*KM**2/SEC**2)
C   VD( )   VECTOR STORED DENSITY
C   X       AREOPOTENTIAL ALTITUDE (KM)
C   XL      AREOPOTENTIAL ALTITUDE AT Z-ZL
C   XA      AREOPOTENTIAL ALTITUDE AT Z-ZA      (KM)
C   XB      AREOPOTENTIAL ALTITUDE AT Z-ZB
C   XF      AREOPOTENTIAL ALTITUDE AT Z-ZF
C   Z       ALTITUDE OF SPACECRAFT ABOVE REFERENCE SURFACE (KM)
C   Z6      ALTITUDE OF 6.1 MB PRESSURE, EQUAL ZERO (KM)
C   ZL      BEGINNING ALTITUDE OF TROPOSPHERE (KM)
C   ZA      BEGINNING ALTITUDE OF STRATOSPHERE (KM)
C   ZB      ALTITUDE OF END OF STRATOSPHERE (KM)
C   ZF      ALTITUDE OF THERMOSPHERIC SURFACE (KM)
C *****
C   DIMENSION PP(9),TINF(3),ZF(3),F(9),DZDS(3),VD(3)
C   DOUBLE PRECISION MB,MBAR,MBOK,NBDNS(9),MW(9),K,LWFCTR,MARSRAD
C   DATA A,AF,AVOGR,ED,ES/2.279D8,6.0D1,0.1660081676D-20,.1d0,.1d0/
C   DATA F/.93d0,.2d-1,.27d-1,.16d-1,.1d-1,.13d-2,5.D-5,1.0D-6,4.0D
C   & -6/
C   DATA K,MW/8.31439d3,44.01d0,1.6d1,28.012d0,39.948d0,28.01d0,
C   & 3.2d1,4.0d0,1.0d0,2.0d0/
C   DATA MBAR,NC,PERIOD,PI,PI2/43.3d0,9,6.8698d2,3.14159265d0,
C   & 6.28318531d0/
C   DATA P6,RA,RB,RC,DTR/6.10D2,3.39467D3,3.39321D3,3.37678D3,
C   & 0.17453292D-1/
C   DATA REFDAT,SIGMA,SOLDAY,U/2.443951D6,1.d0,3.6525636D2,
C   & .42828443D10/

```

```

C ... CONVERT COORDINATES SYSTEM .....
c      write(*,33)chgt,clat,clon,marsrad
c      write(*,44)sunlat,sunlon,als,h
c      write(*,45)upfctr,lwfctr,pres,rsc
33      format(' chgt=',gl2.4,' clat=',gl2.4,' clon=',gl2.4,
& ' marsrad=',gl2.4)
44      format(' sunlat=',gl2.4,' sunlon=',gl2.4,' als=',gl2.4,
& ' h=',gl2.4)
45      format(' upfctr=',gl2.4,' lwfctr=',gl2.4,' pres=',gl2.4,
& ' rsc=',gl2.4,/)
      SNLONG = DTR*SUNLON
      SNLAT = DTR*SUNLAT
      SCLAT = DTR*CLAT
      SCLONG = DTR*CLON
      RSN = MARSRAD
      ELON = DTR*(CLON + 1.085D2)
      COSLAT = DCOS(SCLAT)
      IF(COSLAT.LE.0.0)COSLAT = 0.0
      RSQ = (COSLAT*DCOS(ELON)/RA)**2 + (COSLAT*DSIN(ELON)/RB)**2
& + (DSIN(SCLAT)/RC)**2
      R61MB = DSQRT(1.0D0/RSQ)
      RSC = R61MB + CHGT
C ... CALCULATE LOCAL TIME .....
      DL=SCLONG-SNLONG
      TIME=PI+DL
      IF( TIME.LT.0. ) TIME=TIME+PI2
      IF( TIME.GE.PI2 ) TIME=TIME-PI2
      SCLONG=SCLONG+1.085D2*DTR
C ... CALCULATE THE FRACTION OF HELIOCENTRIC PERIOD .....
      DT=DATE-REFDAT
      FP=DMOD(DT,PERIOD)/PERIOD
      IF( FP.LT.0. ) FP=1.d0+FP
      DAYS=DMOD(DATE-2.443935D6,2.635D1)
      IF( DAYS.LT.0. ) DAYS=DAYS+2.635d1
      AOR = A/RSN
      R61MB=R61MB-2.8D0*DSIN((ALS-5.9D1)*DTR)
C ... CALCULATE THE INCREMENT OF DUST STORM .....
      DL1=ALS-2.10D2
      DL2=ALS-2.70D2
      IF( DL1.LT.0. ) DL1=DL1+3.60D2
      IF( DL2.LT.0. ) DL2=DL2+3.60D2
      DZ1=7.5D0*(1.0D0-DEXP(-DL1/5.0D0))*DEXP(-DL1/35.0D0)/6.5D-01
      DZ2=1.35D1*(1.0D0-DEXP(-DL2/5.0D0))*DEXP(-DL2/35.0D0)/6.5D-01
      DZDS(1)=DZ1+DZ2+1.2d0
C ... CALCULATE THE DIURNAL AND SEASONAL EFFECT .....
      DZSN=ED*DCOS(TIME-3.6651914d0)*DCOSLAT+ES*DCOS(SNLAT-SCLAT)
C ... CALCULATE F10.7 AND TEMPERATURE .....
      Y=(DATE-2.442870D6)*PI2/(1.104D1*SOLDAY)
      F107=7.5D1+AF*(1.0D0-DCOS(Y+3.0D1*DTR*(1.0D0-DCOS(Y))))
      B=1.1D-03*F107
      F107=F107*(1.0D0+B*DSIN(PI2*DAYS/2.635D1))
      T6=2.20D2*AOR
      TA=1.40D2*AOR
      TB=TA
      TF=1.725D2*AOR
C ... CALCULATE PARAMETERS AT POINTS L,A,B,F .....

```

```

F(2)=2.0D-02*(1.0D0-0.5D0*DSIN(TIME)*DSQRT(COSLAT))
F(1)=0.9457D0-F(2)
Z6=0.
DZDS(2)=DZDS(1)+3.0d0*SIGMA
DZDS(3)=DZDS(1)-3.0d0*SIGMA
IF( DZDS(3).LT.0. ) DZDS(3)=0.
TINF(1)=2.05D2*AOR*AOR*((F107+7.5D1)/1.50D2)
TINF(2)=TINF(1)*(1.d0+0.16d0*SIGMA)
TINF(3)=TINF(1)*(1.d0-0.16d0*SIGMA)
ZF(1)=DZDS(1)+1.25D2*AOR + DZSN
ZF(2)=ZF(1)-3.0d0*SIGMA
ZF(3)=ZF(1)+3.0d0*SIGMA
MBOK=1.0D1*MBAR/K
G6=U/R61MB**2
H6=MBOK*G6/T6
IC=0
Z=RSC-R61MB
G=U/(RSC*RSC)
DO 10 M=1,3
  ZL=DZDS(M)/(1.d0-TA/T6)
  ZA=ZL+3.2D1*AOR
  ZB=DZDS(M)+1.0D2*AOR
  GL=U/(R61MB+ZL)**2
  GA=U/(R61MB+ZA)**2
  GB=U/(R61MB+ZB)**2
  XL=(ZL-Z6)*(R61MB+Z6)/(R61MB+ZL)
  XA=(ZA-ZL)*(R61MB+ZL)/(R61MB+ZA)
  XB=(ZB-ZA)*(R61MB+ZA)/(R61MB+ZB)
  TPL=(TA-T6)/XA
  EL=MBOK*GL/TPB
  HA=MBOK*GA/TA
  PL=P6*DEXP(-XL*H6)
  PA=PL*(T6/TA)**EL
  PB=PA*DEXP(-XB*HA )
  GF=U/(R61MB+ZF(M))**2
  XF=(ZF(M)-ZB)*(R61MB+ZB)/(R61MB+ZF(M))
  TPB=(TF-TB)/XF
  EB=MBOK*GB/TPB
  PF=PB*(TB/TF)**EB
  AH=TINF(M)/18.0D0
  GFOKT=1.0D1*GF/(K*TINF(M))
  F(7)=TINF(M)*6.3D-9
  TSQ=DSQRT(TINF(M))
  F(9)=TSQ*1.44D-7
  F(8)=TINF(M)*DEXP(-0.5D0*TSQ)*4.0D-5
  IF( TINF(M).GE.400. ) F(8)=TSQ*4.6D-9*DEXP(1.44D3/TINF(M))/
    * (1.0D0+1.44D3/TINF(M))

```

```

C
C ... CALCULATE MASS DENSITY FOR Z < ZF .....
  IF( Z.GT.ZF(M) ) GO TO 5
C   FOR ALTITUDE BETWEEN ZB 6ND ZF .....
  IF( Z.LT.ZB ) GO TO 1
  X=(Z-ZB)*(R61MB+ZB)/(R61MB+Z)
  T=TB+X*TPB
  P=PB*(TB/T)**EB
  GO TO 4

```

```

C      FOR ALTITUDE BETWEEN ZA AND ZB .....
1  IF( Z.LT.ZA ) GO TO 2
    T=TA
    X=(Z-ZA)*(R61MB+ZA)/(R61MB+Z)
    P=PA*DEXP(-X*HA )
    GO TO 4
C      FOR ALTITUDE BETWEEN ZL AND ZA .....
2  IF( Z.LT.ZL ) GO TO 3
    X=(Z-ZL)*(R61MB+ZL)/(R61MB+Z)
    T = T6 + X*TPL
    P = PL*(T6/T)**EL
    GO TO 4
C      FOR ALTITUDE BETWEEN Z6 AND ZL .....
3  X=(Z-Z6)*R61MB/(R61MB+Z)
    T=T6
    P = P6*DEXP(-X*H6)
4  DENST = 0.1d0*MBOK*P/T
    MB=MBAR
    GO TO 9
C
C ... CALCULATE MASS DENSITY FOR ALTITUDE Z > ZF .....
5  X=(Z-ZF(M))/(1.d0+ (Z-ZF(M))/(RSC-Z+ZF(M)) )
    T=TINF(M)-(TINF(M)-TF)*DEXP(-X/AH)
    TFOT=TF/T
    TKAV=1.0d0/(T*K*AVOGDR)
    DO 6 I=1,NC
        HINF=MW(I)*GFOKT
        PP(I)=PF*F(I)*DEXP(-X*HINF)*TFOT**(AH*HINF)
        NBDNS(I)=PP(I)*TKAV
6  CONTINUE
    SNM2=0.
    P=0.
    DENST=0.
    DO 7 I=1,NC
        P=P+PP(I)
        SNM2=SNM2+NBDNS(I)*MW(I)*MW(I)
        DENST=DENST+NBDNS(I)*MW(I)
        IF( I.EQ.7 ) DNST7=DENST
7  CONTINUE
C
    IF((DENST-DNST7).LT.(50.*DNST7) .OR. IC.EQ.1 ) GO TO 8
    IF( Z.LT.500. ) GO TO 8
    IC=1
    TINFO=TINF(2)
    TINF(2)=TINF(3)
    TINF(3)=TINFO
8  CONTINUE
    MB=SNM2/DENST
    DENST=DENST*AVOGDR
C
9  VD(M)=DENST
    IF( M.NE.1 ) GO TO 10
    TEMP=T
    PRES = P
    H=0.1d0*K*T/(MB*G)
10 CONTINUE

```

C

```
DENST=VD(1)
UPFCTR=VD(2)/VD(1)
LWFCTR=VD(3)/VD(1)
IF( Z.GT.ZA ) RETURN
UPFCTR=1.d0+(0.1d0+ 1.45d0*Z/ZB ) * SIGMA
LWFCTR=0.9d0 - SIGMA*0.145D-1*Z/(ZA-ZL)
return
END
```

```
function rand(i)
C... Function to compute random number uniformly distributed
C between 0 and 1
C.....
double precision x,rand
C... static x
if(i.ne.0) x = i/2.62144D+05
x = x*5.09D2
x = x - Dint(x)
rand = x
return
end
```

```
subroutine normal(d1,d2)
C... SUBROUTINE to compute a pair of normally (Gaussian) distributed
C variables with mean value 0 and standard deviation 1
C.....
implicit double precision (a-h,o-z)
50 x = rand(0)
y = 2.D0*rand(0) - 1.
xx = x**2
yy = y**2
s = xx + yy
if(s-1)51,51,50
51 al = dsqrt(-2.*dlog(rand(0)))/s
d1 = (xx - yy)*al
d2 = 2.D0
return
end
```

APPENDIX B - DOCUMENTATION FOR THE MARS/ATMOS PROGRAM

The MARS/ATMOS program is invoked in interactive mode by entering MARS. An example of the program interactive operation is shown as Table B-1. The user may select filenames (or CON for console output) for a LIST file and an OUTPUT file. Examples of the LIST and OUTPUT files are shown in Tables B-2 and B-3. The LIST file has self-explanatory labels. The OUTPUT file contains data suitable for reading into auxiliary programs, and consists of: height (km), latitude (degrees), longitude (degrees), log-base-10 of density (kg/m^3), temperature (K), eastward wind (m/s), northward wind (m/s), and density perturbation magnitude (% , defined as high density minus low density divided by twice the average density).

Other output files, suitable for plotting, contain x, y pairs of values, where x may be selected as height, latitude or longitude and y is either log-base-10 of low density (DENSLO file), log-base-10 of average density (DENSAV file), log-base-10 of high density (DENSHE file), log-base-10 of density-plus-perturbation (DENSHP file), temperature (TEMP file), pressure (PRES file), eastward wind (EWWIND file), or northward wind (NSWIND file). A sample of the DENSAV file is shown in Table B-4.

The user is prompted (see Table B-1) to enter the month, day of month, year and maximum number of positions to compute. If the maximum number of positions is input as zero, position data (time, height, latitude, longitude) is read from a file called TRAJDATA. Otherwise the program steps linearly through height, latitude, and/or longitude for the desired number of positions. Greenwich Mean time for the starting position is input in hours, minutes and seconds. All solar and Mars orbital positions are computed by the program from the date and time input.

The program computes random perturbations in density, relative to the average density and with perturbation magnitudes evaluated from the low and high density values. A starting random number (any odd positive integer) must be input to start the random perturbation sequence. If a different number is selected, a different sequence will be generated; if the same starting random number is selected, the same random sequence will be selected.

A parameter value of 1, 2 or 3 is input to select plot output files (DENSAV file, etc.) versus height, latitude, or longitude respectively. For plotting variables versus height, option 1 is selected (see Table B-4).

Initial height (km), latitude (degrees, N++, S--) and longitude (0-360° E) must be input, along with increments of height, latitude, longitude and time for the program-generated position sequence. Increments may be positive (increasing value with position step) or negative (decreasing value with position step).

The program is terminated by entering zero or negative values for initial date and number of positions.

TABLE B-1

SAMPLE INTERACTIVE OPERATION OF MARS/ATMOS PROGRAM

```

MARS
Enter name for LIST file (CON for console listing):
MARSLIST
Enter name for OUTPUT file:
MARSOUT
Enter Month, Day of Month, 4-digit Year, and Max Number Positions
7 20 1976 13
Enter initial GMT Time (Hours, Minutes, Seconds)
0 0 0

Enter Starting Random Number (Any odd positive integer)
123

Enter 1, 2 or 3 for output versus Height, Latitude, or Longitude, respectively
1
Enter Initial Height (km), Latitude (deg.), Longitude (deg.)
600 22.23 312.07
Enter Increments in Height (km), Latitude (deg.), Longitude (deg.),
and Time (sec.)
-50 0 0 0
Computing data.
Enter Month, Day of Month, 4-digit Year, and Max Number Positions
0 0 0 0
Normal Termination

```


TABLE B-2

PRINTOUT OF MARSLIST LIST FILE

Date = 7/20/1976 Julian Date = 2442980. GMT Time = 0: 0: .0
 Starting random number = 123
 TIME (relative to initial time) = .0 seconds
 HEIGHT = 600.0 km SCALE HEIGHT = 428.53 km
 LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
 TEMPERATURE = 168.7 K
 DENSITY (Low, Avg., High) = .1513E-15 .3224E-15 .9169E-15 kg/m**3
 DENSITY PLUS PERTURBATION = .1597E-14 kg/m**3
 PRESSURE = .4204E-09 N/m**2
 EASTWARD WIND = .0 m/s NORTHWARD WIND = .5 m/s

TIME (relative to initial time) = .0 seconds
 HEIGHT = 550.0 km SCALE HEIGHT = 354.96 km
 LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
 TEMPERATURE = 168.7 K
 DENSITY (Low, Avg., High) = .2795E-15 .3659E-15 .6832E-15 kg/m**3
 DENSITY PLUS PERTURBATION = .9299E-15 kg/m**3
 PRESSURE = .4671E-09 N/m**2
 EASTWARD WIND = .0 m/s NORTHWARD WIND = .5 m/s

TIME (relative to initial time) = .0 seconds
 HEIGHT = 500.0 km SCALE HEIGHT = 220.23 km
 LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
 TEMPERATURE = 168.7 K
 DENSITY (Low, Avg., High) = .3199E-15 .4357E-15 .1002E-14 kg/m**3
 DENSITY PLUS PERTURBATION = .1632E-14 kg/m**3
 PRESSURE = .5225E-09 N/m**2
 EASTWARD WIND = .0 m/s NORTHWARD WIND = .4 m/s

TIME (relative to initial time) = .0 seconds
 HEIGHT = 450.0 km SCALE HEIGHT = 96.39 km
 LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
 TEMPERATURE = 168.7 K
 DENSITY (Low, Avg., High) = .3775E-15 .6165E-15 .2109E-14 kg/m**3
 DENSITY PLUS PERTURBATION = .3254E-14 kg/m**3
 PRESSURE = .5954E-09 N/m**2
 EASTWARD WIND = .0 m/s NORTHWARD WIND = .4 m/s

TIME (relative to initial time) = .0 seconds
 HEIGHT = 400.0 km SCALE HEIGHT = 45.41 km
 LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
 TEMPERATURE = 168.7 K
 DENSITY (Low, Avg., High) = .5169E-15 .1367E-14 .6605E-14 kg/m**3
 DENSITY PLUS PERTURBATION = .8583E-14 kg/m**3
 PRESSURE = .7277E-09 N/m**2
 EASTWARD WIND = -.1 m/s NORTHWARD WIND = .4 m/s

TIME (relative to initial time) = .0 seconds
 HEIGHT = 350.0 km SCALE HEIGHT = 31.88 km
 LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees

TEMPERATURE = 168.7 K
DENSITY (Low, Avg., High) = .1239E-14 .5334E-14 .2647E-13 kg/m**3
DENSITY PLUS PERTURBATION = .4095E-13 kg/m**3
PRESSURE = .1153E-08 N/m**2
EASTWARD WIND = -.6 m/s NORTHWARD WIND = .6 m/s

TIME (relative to initial time) = .0 seconds
HEIGHT = 300.0 km SCALE HEIGHT = 28.20 km
LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
TEMPERATURE = 168.7 K
DENSITY (Low, Avg., High) = .6768E-14 .2875E-13 .1205E-12 kg/m**3
DENSITY PLUS PERTURBATION = .1240E-12 kg/m**3
PRESSURE = .3283E-08 N/m**2
EASTWARD WIND = -2.7 m/s NORTHWARD WIND = 1.6 m/s

TIME (relative to initial time) = .0 seconds
HEIGHT = 250.0 km SCALE HEIGHT = 25.69 km
LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
TEMPERATURE = 168.7 K
DENSITY (Low, Avg., High) = .5611E-13 .1827E-12 .6238E-12 kg/m**3
DENSITY PLUS PERTURBATION = .6101E-12 kg/m**3
PRESSURE = .1642E-07 N/m**2
EASTWARD WIND = -11.4 m/s NORTHWARD WIND = 6.1 m/s

TIME (relative to initial time) = .0 seconds
HEIGHT = 200.0 km SCALE HEIGHT = 17.80 km
LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
TEMPERATURE = 168.7 K
DENSITY (Low, Avg., High) = .6587E-12 .1725E-11 .5145E-11 kg/m**3
DENSITY PLUS PERTURBATION = .4576E-11 kg/m**3
PRESSURE = .1221E-06 N/m**2
EASTWARD WIND = -41.1 m/s NORTHWARD WIND = 34.7 m/s

TIME (relative to initial time) = .0 seconds
HEIGHT = 150.0 km SCALE HEIGHT = 10.22 km
LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
TEMPERATURE = 168.5 K
DENSITY (Low, Avg., High) = .5150E-10 .8682E-10 .1779E-09 kg/m**3
DENSITY PLUS PERTURBATION = .1842E-09 kg/m**3
PRESSURE = .3323E-05 N/m**2
EASTWARD WIND = 47.1 m/s NORTHWARD WIND = 33.6 m/s

TIME (relative to initial time) = .0 seconds
HEIGHT = 100.0 km SCALE HEIGHT = 7.64 km
LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
TEMPERATURE = 139.8 K
DENSITY (Low, Avg., High) = .2191E-07 .2642E-07 .4082E-07 kg/m**3
DENSITY PLUS PERTURBATION = .4446E-07 kg/m**3
PRESSURE = .7089E-03 N/m**2
EASTWARD WIND = 26.9 m/s NORTHWARD WIND = -2.6 m/s

TIME (relative to initial time) = .0 seconds
HEIGHT = 50.0 km SCALE HEIGHT = 6.87 km
LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees

TEMPERATURE = 129.3 K
DENSITY (Low, Avg., High) = .2945E-04 .3577E-04 .5575E-04 kg/m**3
DENSITY PLUS PERTURBATION = .5283E-04 kg/m**3
PRESSURE = .8884 N/m**2
EASTWARD WIND = 12.1 m/s NORTHWARD WIND = -1.2 m/s

TIME (relative to initial time) = .0 seconds
HEIGHT = .0 km SCALE HEIGHT = 10.48 km
LATITUDE = 22.230 degrees EAST LONGITUDE = 312.070 degrees
TEMPERATURE = 203.3 K
DENSITY (Low, Avg., High) = .1193E-01 .1327E-01 .1495E-01 kg/m**3
DENSITY PLUS PERTURBATION = .1465E-01 kg/m**3
PRESSURE = 517.9 N/m**2
EASTWARD WIND = .5 m/s NORTHWARD WIND = .0 m/s

TABLE B-3

PRINTOUT OF MARSOUT OUTPUT FILE

600.0	22.23	312.07	-15.49	168.71	.05	.51	118.74
550.0	22.23	312.07	-15.44	168.71	.04	.48	55.17
500.0	22.23	312.07	-15.36	168.71	.04	.45	78.28
450.0	22.23	312.07	-15.21	168.71	.01	.43	140.42
400.0	22.23	312.07	-14.86	168.71	-.11	.44	222.63
350.0	22.23	312.07	-14.27	168.71	-.58	.63	236.50
300.0	22.23	312.07	-13.54	168.71	-2.65	1.59	197.86
250.0	22.23	312.07	-12.74	168.71	-11.44	6.07	155.35
200.0	22.23	312.07	-11.76	168.71	-41.07	34.65	130.06
150.0	22.23	312.07	-10.06	168.47	47.09	33.65	72.78
100.0	22.23	312.07	-7.58	139.77	26.86	-2.58	35.79
50.0	22.23	312.07	-4.45	129.35	12.14	-1.19	36.77
.0	22.23	312.07	-1.88	203.26	.49	-.05	11.39

TABLE B-4

PRINTOUT OF DENSAV FILE

600.000	-15.49
550.000	-15.44
500.000	-15.36
450.000	-15.21
400.000	-14.86
350.000	-14.27
300.000	-13.54
250.000	-12.74
200.000	-11.76
150.000	-10.06
100.000	-7.578
50.000	-4.446
.000	-1.877